

Optimization of biomass fired grate stoker systems

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Introduction

The TNO mission:

To apply technological knowledge with the aim of strengthening the innovative power of industry

One field of expertise is **Thermal Conversion Technology**

Mathematical models are used to optimize thermal conversion processes, like:

- Cement process
- Biomass gasification
- Biomass combustion
- Municipal Solid Waste Combustion

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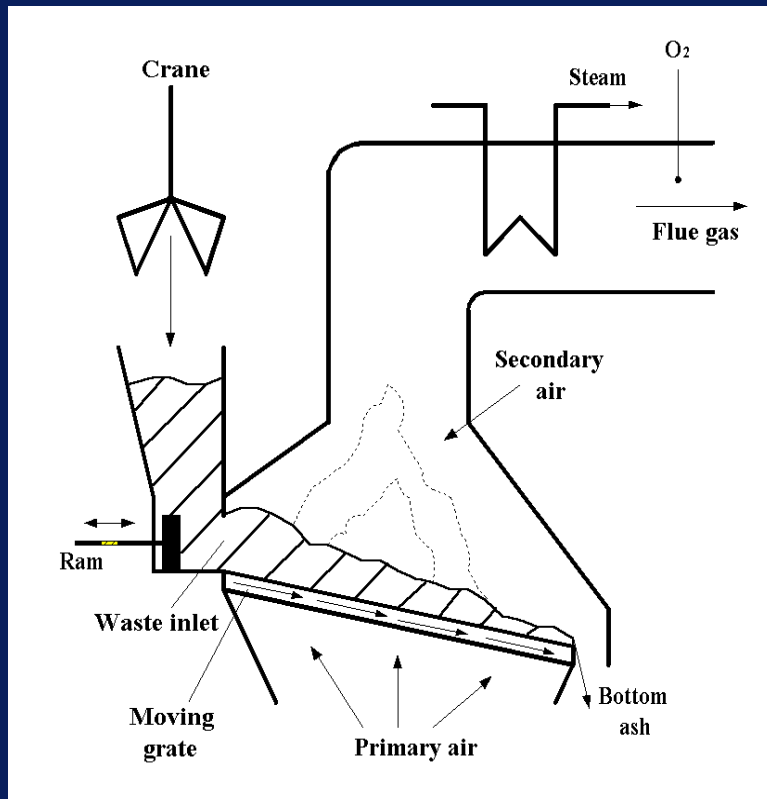
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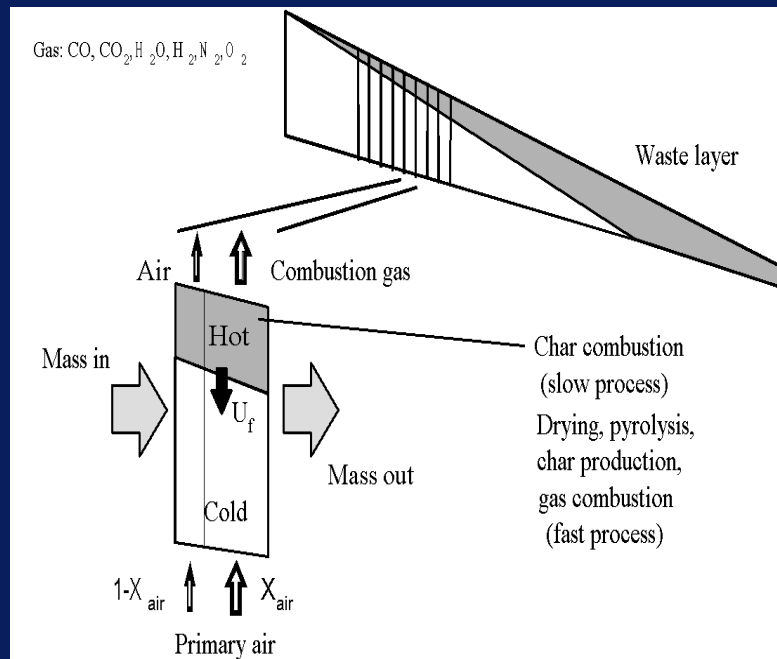
Dynamic model for grate stoker systems (1)



**Dynamics of the furnace:
Fuel layer
Gas phase
and the boiler section are
described**

**Interaction between the gas
phase and the fuel layer
through radiation**

Dynamic model for grate stoker systems (2)



The grate is divided into many slices

Mass and energy balances solved for every slice

Conversion process:

Propagation of ignition front

Fuel layer divided in two parts:

Hot reacting part on top

Cold fresh fuel at the bottom

Speed of propagation front is depending upon:

Fuel composition

Amount of combustion air

Dynamic model for grate stoker systems (3)

Geometry is included:

Co-current part

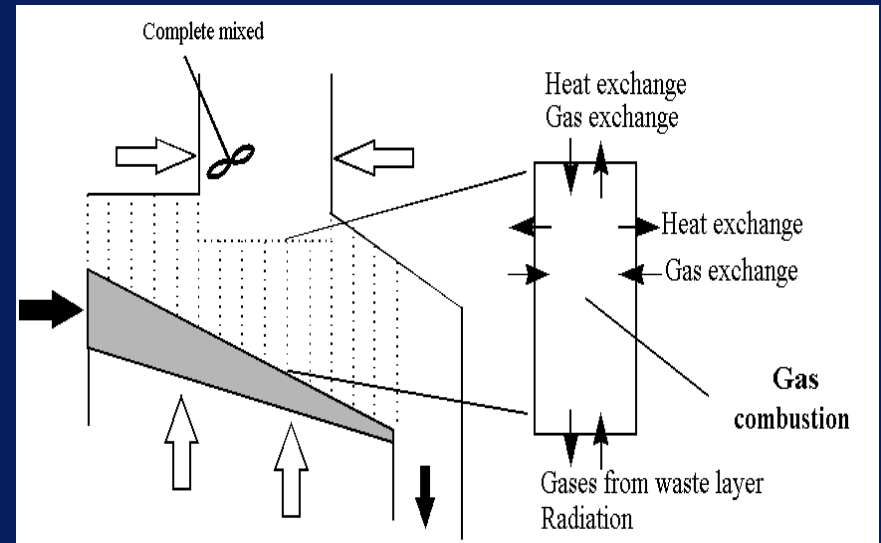
Countercurrent part

Ideally mixed part

The co-current and countercurrent parts are divided into many ideally mixed gas reactors with

CO, H₂: mixed is burnt

Non-ideal mixing parameter



Model validation (1)

How to validate dynamic models?

Step response method

System identification

System identification:

Experimental modeling resulting in dynamic input-output relations without any physical meaning (black-box modeling)

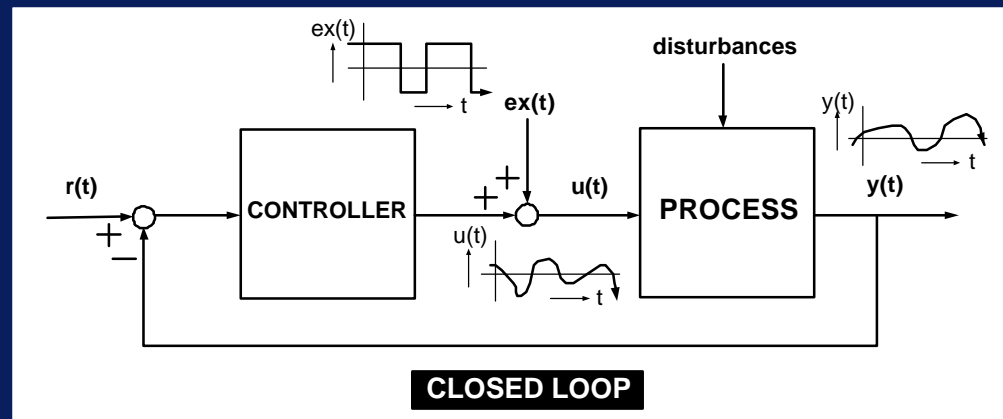
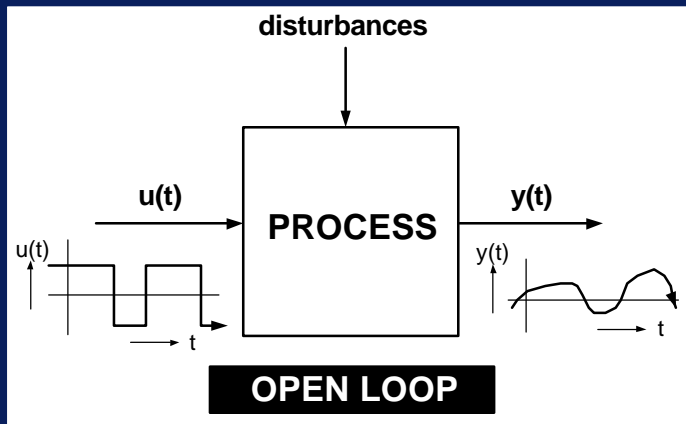
Can be used for MIMO systems and for closed-loop systems.

Model validation (2)

Three step procedure in system identification:

1. Experimental phase

excitation of process by user-defined signals + collection of in- and output data $u(t)$ resp. $y(t)$, $t=1 \dots N$:



2. Estimation of a model

by minimizing the difference between the measured output signals $y(t)$ and prediction of these output signals $y^*(t, \text{parameters})$:

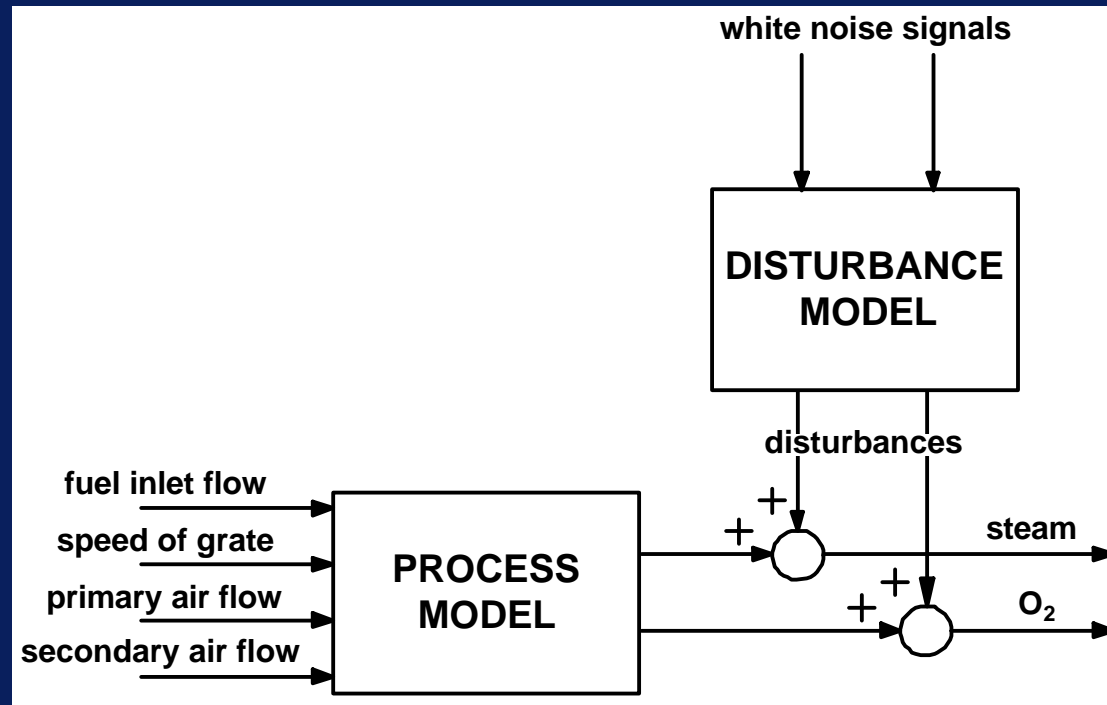
$$\min_{\text{parameters}} \frac{1}{N} \sum_{t=1}^N (y(t) - y^*(t, \text{parameters}))^2$$

3. Validation of the estimated model

by using, for example, statistical techniques

Model validation (3)

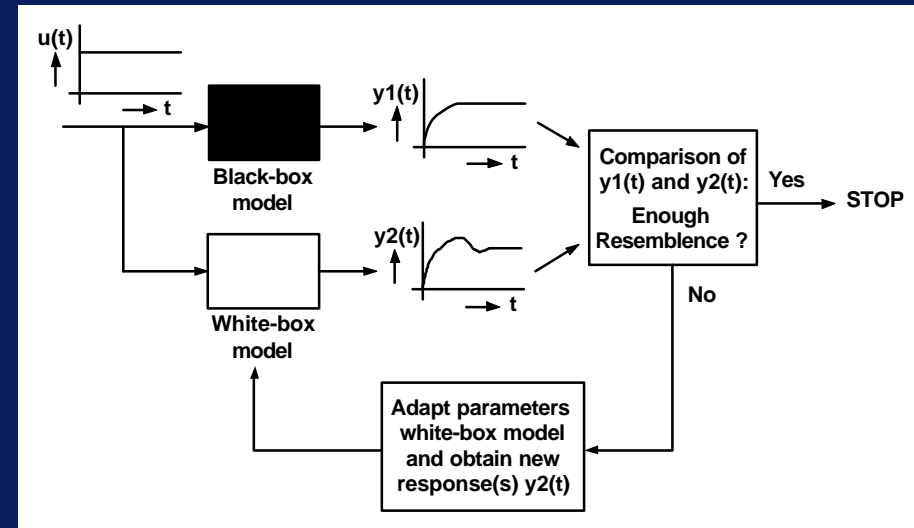
System identification results in a separated process and disturbance model:



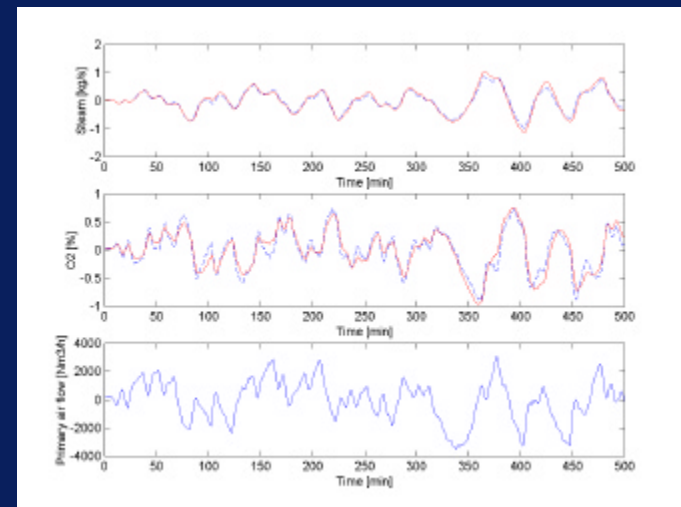
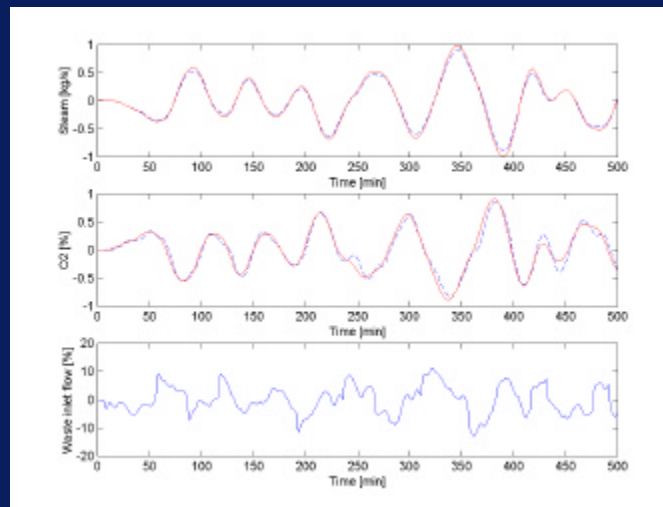
Model validation (4)

Validation first-principles model by means of the estimated model:

Method:



Results:



Practical application (1)

Operational experiences:

fly-ash deposition to the furnace walls, leading to **reduced throughput**.

high fly-ash rates due to a relative small grate and high primary air flows.

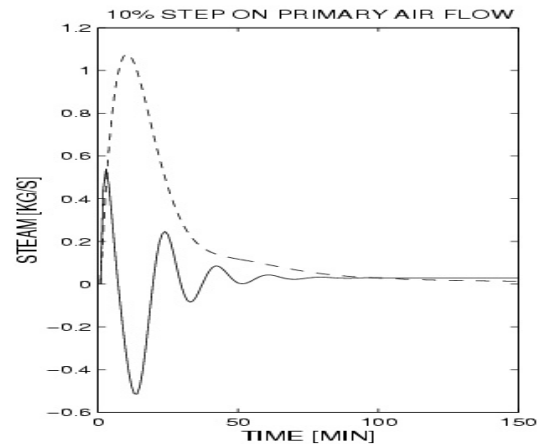
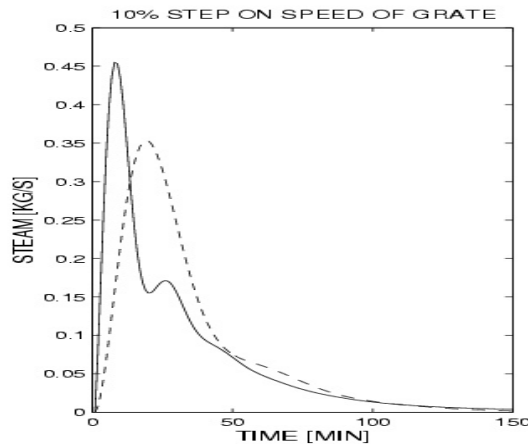
flue gas temperatures at inlet second boiler pass fairly high, causing **high temperature corrosion**.

no reliable combustion of low-calorific fuels.

Practical application (2)

Title:

Process analysis with system identification:



Practical application (3)

Conclusions of process analysis:

Influence primary air is bad due to excess air and wrong distribution

Grate speed is used as control variable

**Control concept is not in agreement with philosophy:
primary air is the best control variable**

Practical application (4)

Application of TNO-simulator:

Adaptation of the model to the specific situation, including control concepts

Conclusion from simulations (1):

Very short fire, high thermal load on zones 1 and 2.

The steam production can be influenced mainly with the waste flow and grate speed. The primary air has nearly no influence.

Oxygen can be controlled well with the primary and secondary air flow.

Practical application (5)

Conclusion from simulations (2):

Present control concept is not transparent, so adaptation is needed

Primary air distribution along the grate has to be changed

A new control concept has been developed based upon experiences with the simulator

Practical application (6)

Control objectives:

Maximal conversion (combustion) of the fuel

Maximal fuel throughput (highly flexible)

Maximal steam production/energy output

Operate below but as close as possible to the maximum levels imposed out of life span considerations

Reduce the fluctuations in the process variables due to the variation in fuel composition:

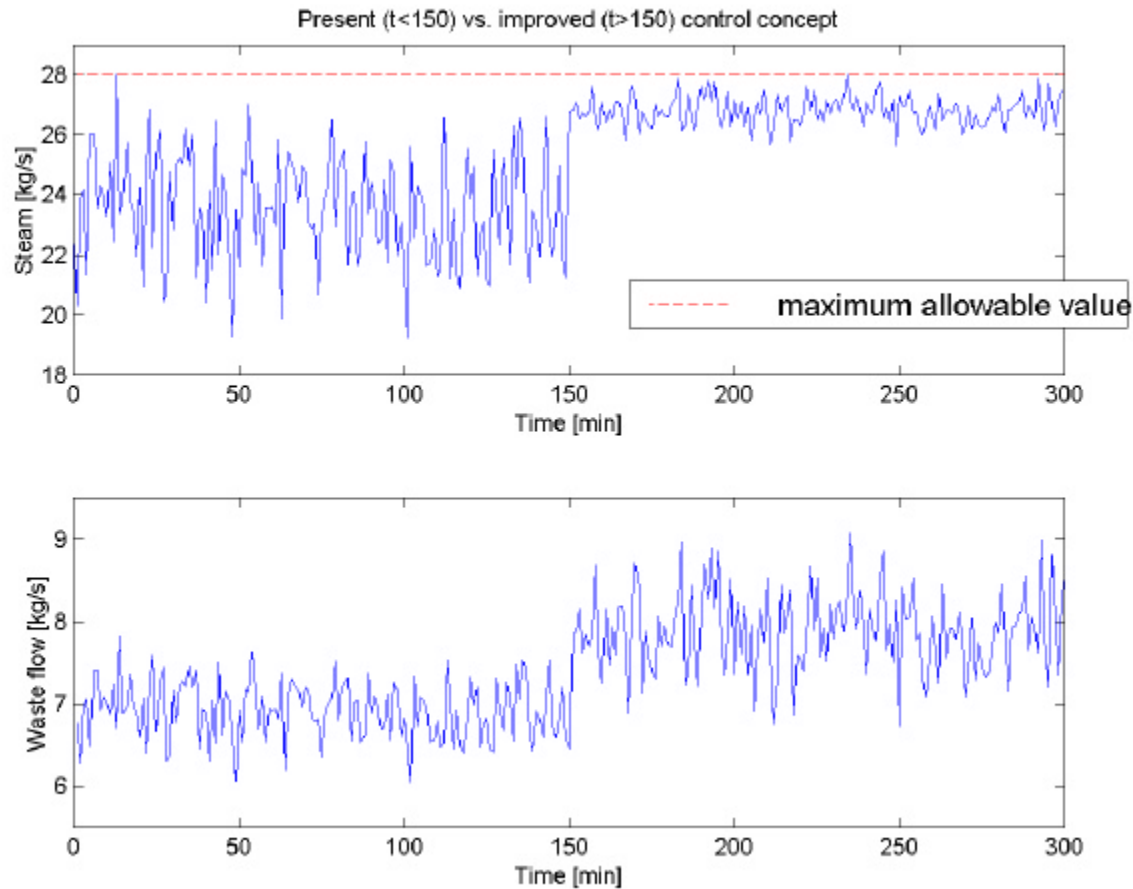
- Reduce fatigue due to variability of thermal stress

- To be able to operate more closely to constraints imposed out of life span considerations

- To reduce load on post-combustion control equipment

Practical application (7)

Results:



Control of solid fuel combustion plants (1)

Performance assessment conventional solid fuel combustion control systems:

Inefficient control due to:

Complex (multivariable) character of the process

Presence of multiple conflicting control objectives

Not being allowed to exceed certain constraints (limits)

Control of solid fuel combustion plants (2)

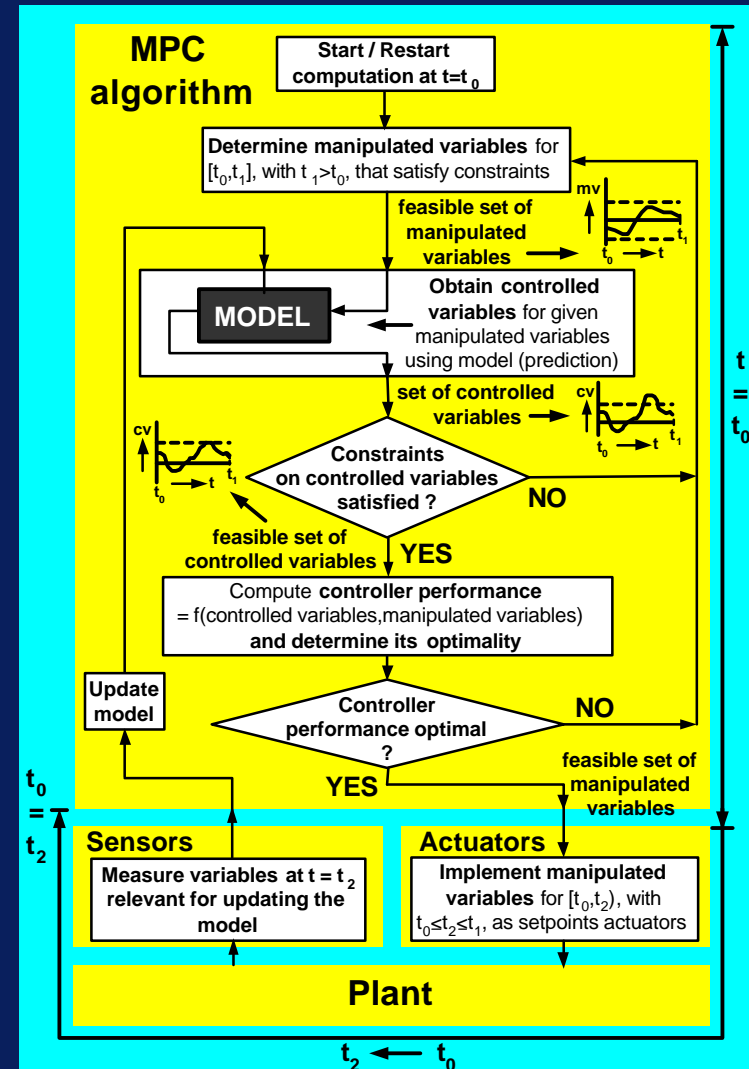
Model Predictive Control:
Computation of manipulated variables via solving on-line, at each sample instant, a mathematical optimization problem

Ingredients:

Dynamic Model

Objective function: reflects controller performance

Constraints



OPTICOMB Project (1)

Optimization and design of biomass combustion systems

Objective:

Increasing flexibility of fuels and reducing emissions

Expected results:

Reduction of emissions

Innovative control concepts

New grate system

New furnace concept

OPTICOMB Project (2)

Sponsored by EU. Start January 2003. Duration 3.5 years

Coordination: TNO

Partners: **University of Graz**
 Eindhoven University
 Vyncke
 University of Lisbon
 National Swedish Research Institute
 Bio-energy plant Schijndel

Conclusions

A dynamical first principal model of grate firing systems is available

Validation has shown that the model is in good compliance with practical data

The model forms a good basis for improvement of combustion systems, in specific with respect to the control concept

Results have been demonstrated at biomass combustion systems

Development of MPC has been started