



# Ash Deposition Prediction Tool for PF Boilers Fired with Coal and Biomass

Piotr Plaza, Cardiff University, TU Delft

Tony Griffiths, Cardiff University

Yash Joshi, Wiebren de Jong, TU Delft

Mark Mulder, E.ON Benelux

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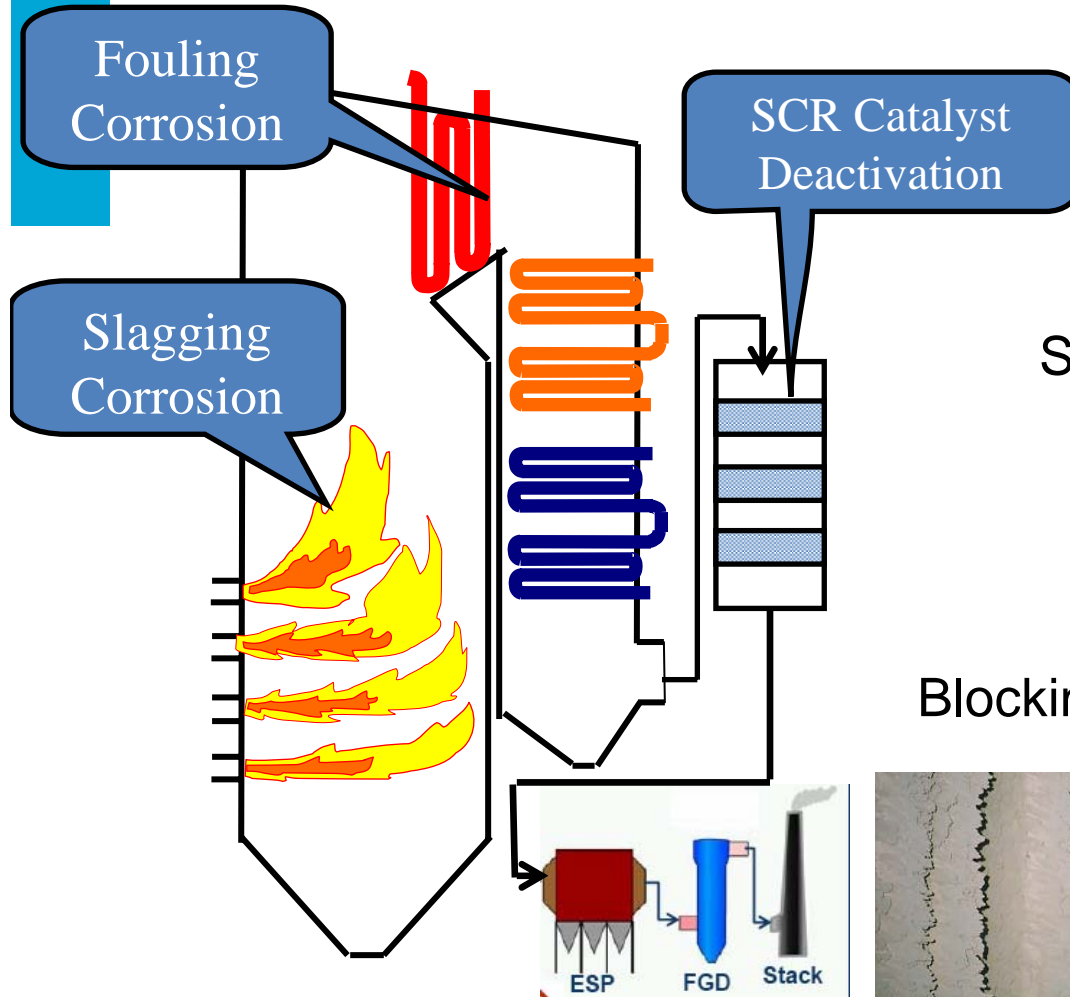
- Model requirements
- Zonal Method -> Boiler Thermal Performance
- Ash Deposition Modelling -> Thermo-chemical Mechanistic Approach

## 3. Case study: 230 MWe PF Boiler

- Results for Coals and Co-firing with Biomass
  - focus on boiler performance (wet fuels)
  - ash deposition assessment risks (blends with straw, olive residues, sawdust)

## 4. Recommended Fuel Blends -> importance of coal ash quality

# Ash-related Problems



## Slagging (1600-1300°C)

Molten or semi-fused ash

## HT Fouling (1300-900°C)

Semi-fused ash & sintered deposits

## LT Fouling (900-400°C)

Loose or slightly sintered deposits

## DeNOx Fouling&Poisoning

Blocking/poisoning of catalyst active sites



Silicates

Salts

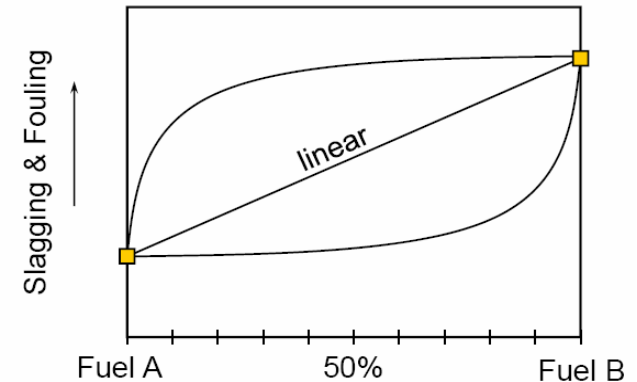
# Current Models / Model Requirements

## Slagging/fouling indices

- Mostly developed for coal combustion (limited to the range of coals)

## CFD – Based models / simulators

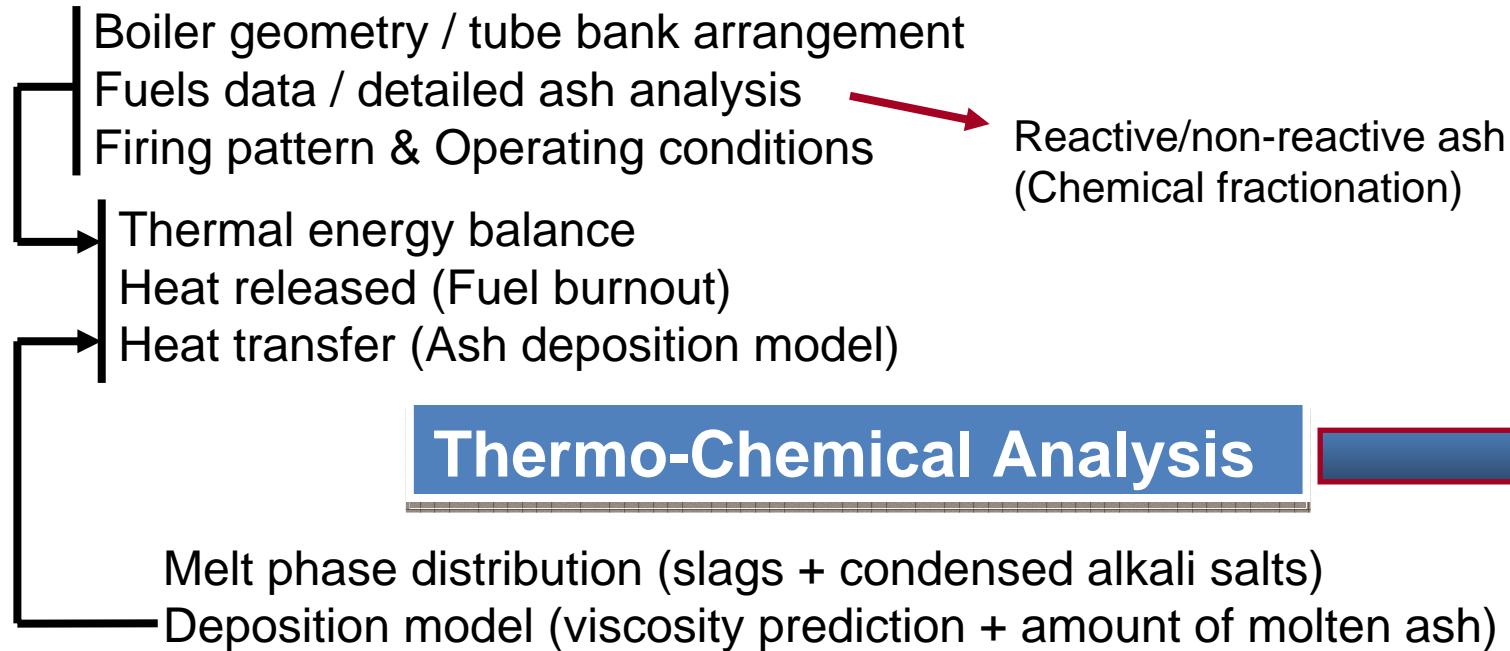
- Time consuming, highly skilled
- Detailed ash deposition models are still under development (post-processors)



## What is Needed

- Generic model => An Engineering Advisory Tool
- Easily adaptable model => various geometry and operating conditions
- Various fuel types => use of a comprehensive thermodynamic data (slag/solid/gas-phase=>FactSage)

# ZONE-BASED MODEL - Temperature Profile (1D)

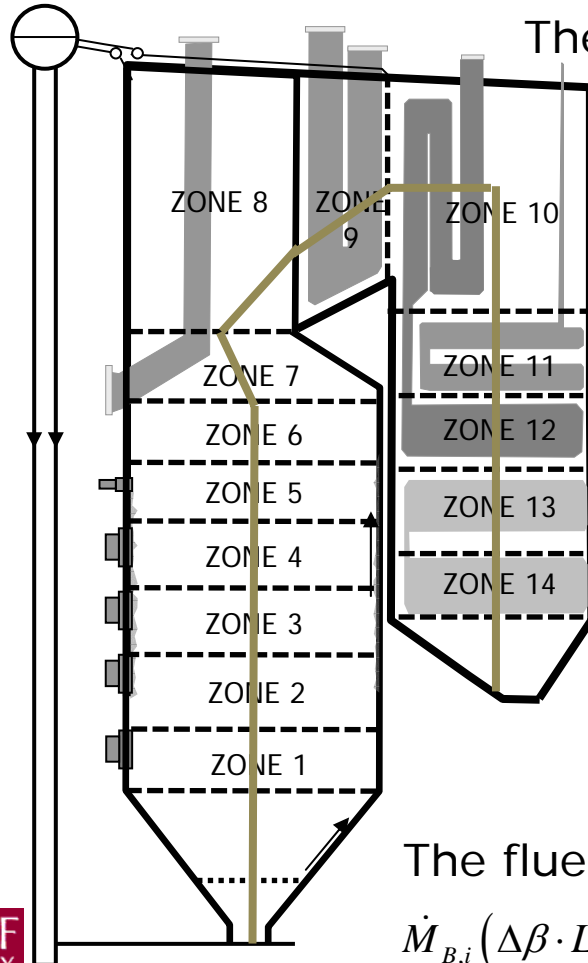


## POTENTIAL BOILER INDICATOR

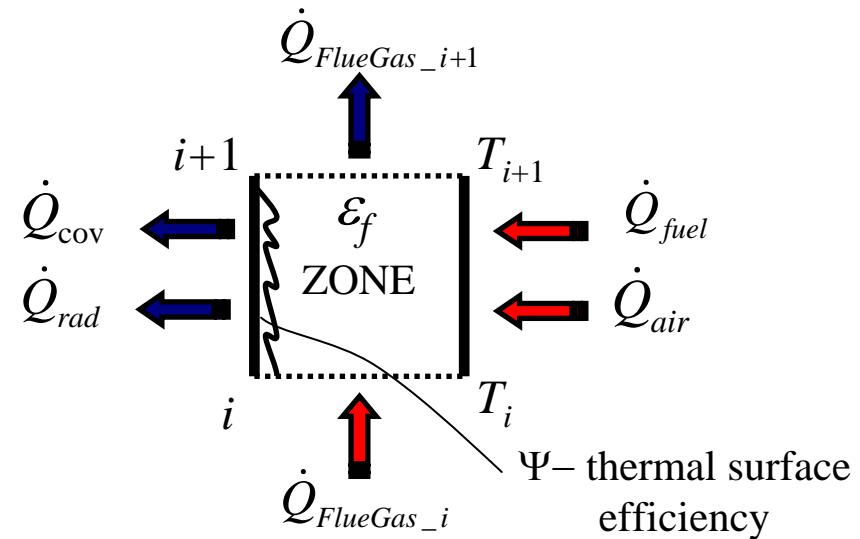
- **SLAGGING**
- **FOULING**
- **Boiler Efficiency**
- **Boiler's operational parameters**

Simulation of deposit build-up  
Direct impact of deposition on boiler performance

# Zone-based Model



Thermal energy balance of a zone in the furnace:

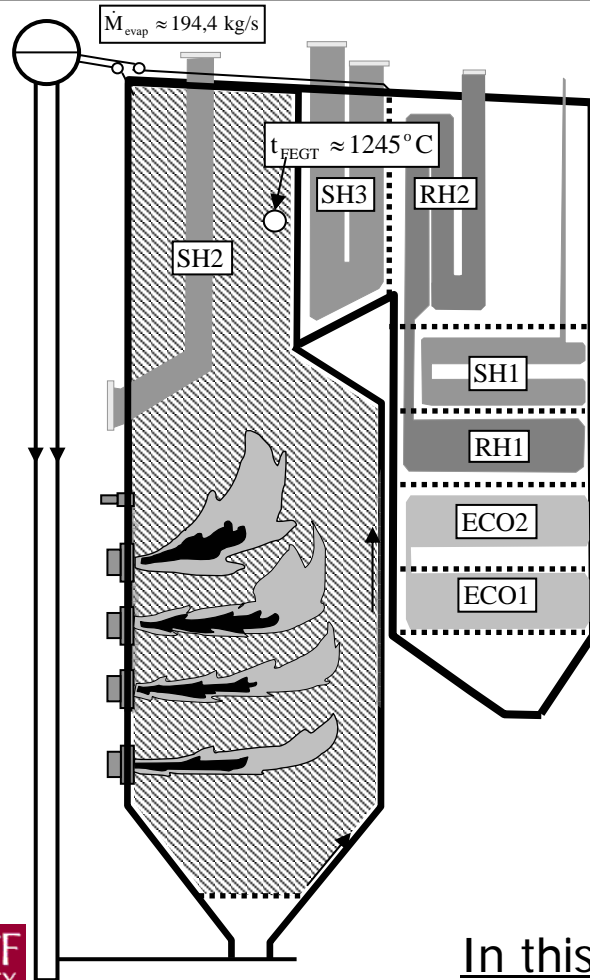


$$\dot{Q}_{FlueGas\_i} + \dot{Q}_{fuel} + \dot{Q}_{air} - \dot{Q}_{rad} - \dot{Q}_{cov} - \dot{Q}_{FlueGas\_i+1} = 0$$

The flue gas temperature at the outlet of the furnace:

$$t_{i+1} = \frac{\dot{M}_{B,i} (\Delta\beta \cdot LHV + i_f) + Q_{Air,i}}{\dot{M}_{B,i+1} VC_{i+1}} + \frac{\dot{M}_{B,i} VC_i}{\dot{M}_{B,i+1} VC_{i+1}} t_i - \frac{\sigma_0 \epsilon_f}{\dot{M}_{B,i+1} VC_{i+1}} \left[ 0.5 (T_i^4 + T_{i+1}^4) \right] \times (\Psi F)$$

# Case study: 230MWe PF Boiler



The coal burned was a blend of

- South African
- Australian
- Colombian Coal

Secondary fuels considered for co-firing

- Sawdust -> up to 60<sup>th</sup>%
- Straw -> up to 30<sup>th</sup>%
- Olive Residues -> up to 30<sup>th</sup>%
- Sewage Sl. -> up to 10<sup>th</sup>%

In this study no biomass fuels mixtures were investigated!

# Investigated Fuels

Fuel property	Colombian Coal – CO1	South African Coal – SA1	Australian Coal– AL1	Sawdust SD2/SD2wet	Olive Residue – OR3	Sewage Sludge – SL1	Danish Straw – DS2
LHV,(ar) kJ/kg	26080	24070	22160	17630 / 10480	16400	9100	14670
Proximate analysis (% as received basis)							
Volatile Matter (VM)	34.03	24.52	28.30	77.43 / 49.94	66.24	36.72	68.49
Fixed Carbon (FC)	48.17	52.58	43.70	14.85 / 9.58	14.92	2.75	13.15
Moisture	9.00	6.30	3.30	<b>6.98 / 40.00</b>	9.00	11.72	12.40
Ash	8.80	16.60	24.70	0.74 / 0.48	9.84	<b>48.81</b>	<b>5.96</b>
AFM Composition (g/ kg fuel)							
Si	25.42	32.51	55.65	0.74	13.31	79.63	9.47
Al	9.83	25.83	41.31	0.09	1.56	31.52	0.30
Fe	4.06	8.36	13.65	0.15	2.71	64.87	0.27
Ca	1.38	8.66	6.71	2.35	<b>16.37</b>	40.12	3.11
<b>K</b>	1.75	0.96	0.82	0.84	<b>14.16</b>	10.94	<b>14.74</b>
<b>Na</b>	0.72	0.74	0.37	0.05	3.31	3.98	0.38
P	0.08	0.00	0.54	0.1	1.46	<b>30.89</b>	0.74
Cl	0.10	0.10	0.10	0.1	<b>9.10</b>	1.0	<b>4.82</b>





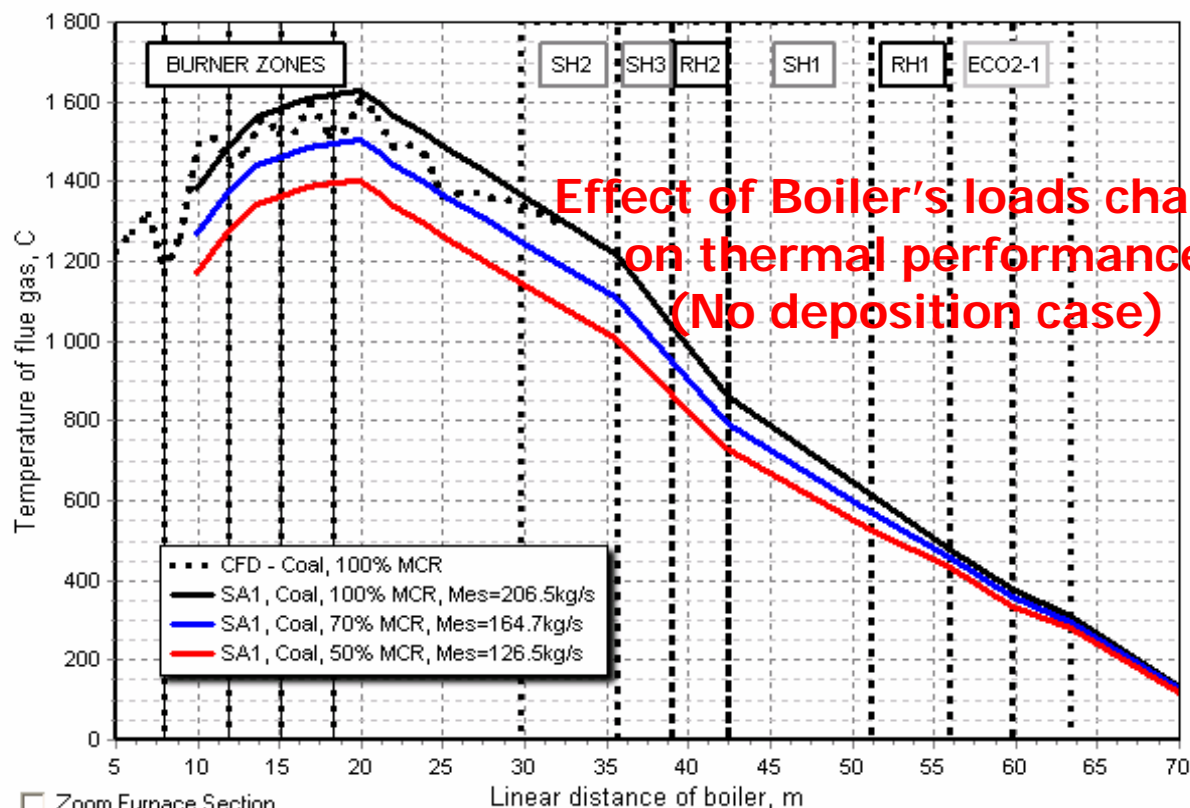
# SLAGGING PREDICTOR



BLEND CALCULATOR | BOILER | 1D TEMP PROFILE | SLAGGING/FOULING | SALTS DEPOSITION | HEAT TRANSFER | INDICATORS

Temperature Profiles | Heat Flux | Thermal Efficiency Factors | Furnace Wall Temperatures | Wykresy

Flue Gas Side | Water/Steam Side



Co-firing Options  
 Bi-Fuel  
 Multifuel

Co-firing Rates, %  
 Energy  
 Mass

Parent Fuel %  
SA1  
Substitute Fuel  
SA1 0.0

Update

SLAGGING

FOULING

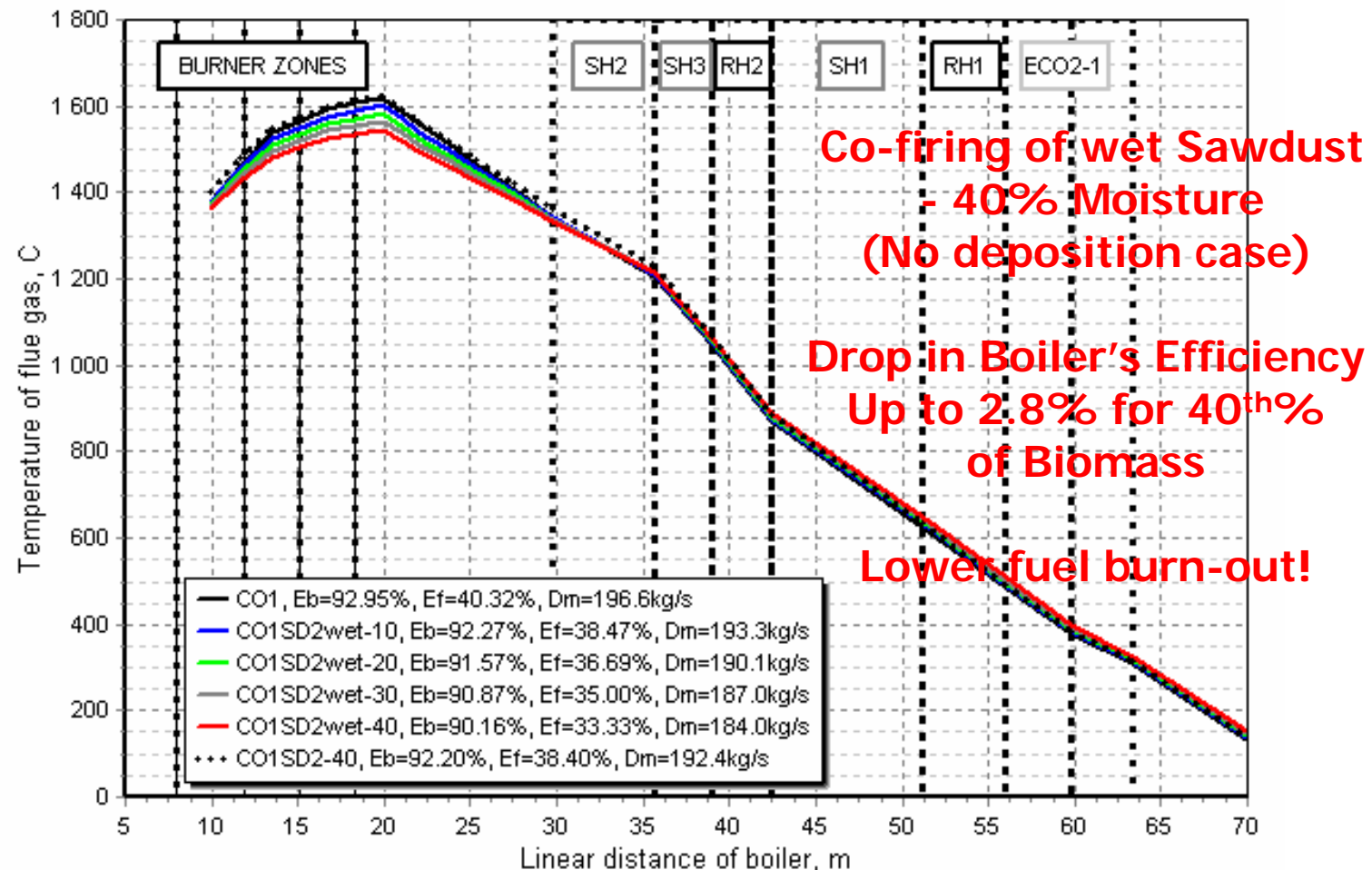
START

SETTINGS

Temp

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# Predicted Thermal Boiler Performance



Heat transfer shifts towards the convective section of boiler

-> lower mass flows of the produced steam.

# Conclusions – No deposition cases

Effect of the high moisture and low/high ash load on thermal boiler performance

## SAWDUST

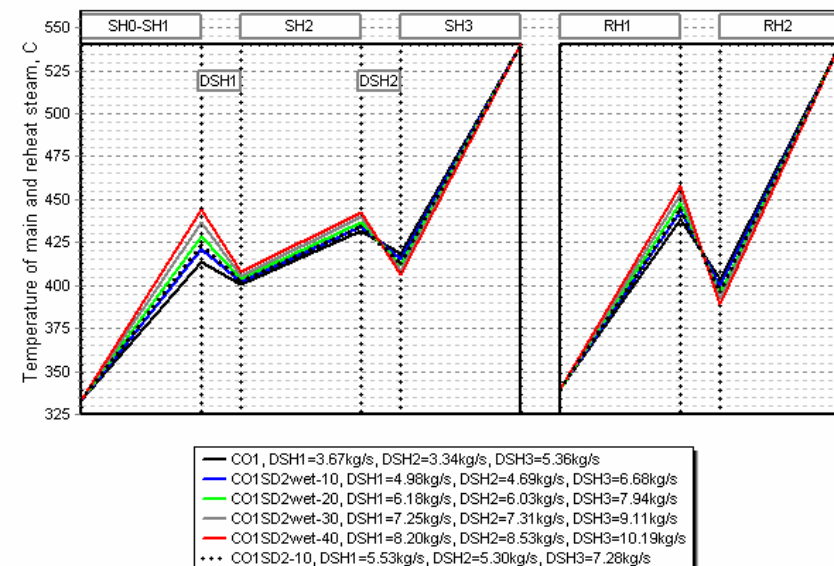
- Co-firing high percentages of wet sawdust may lead to significant drop in boiler efficiency, lower steam generation, and higher steam parameters variations -> resulting in steam overheating and increased spray-water injections into DSH

## SEWAGE SLUDGE

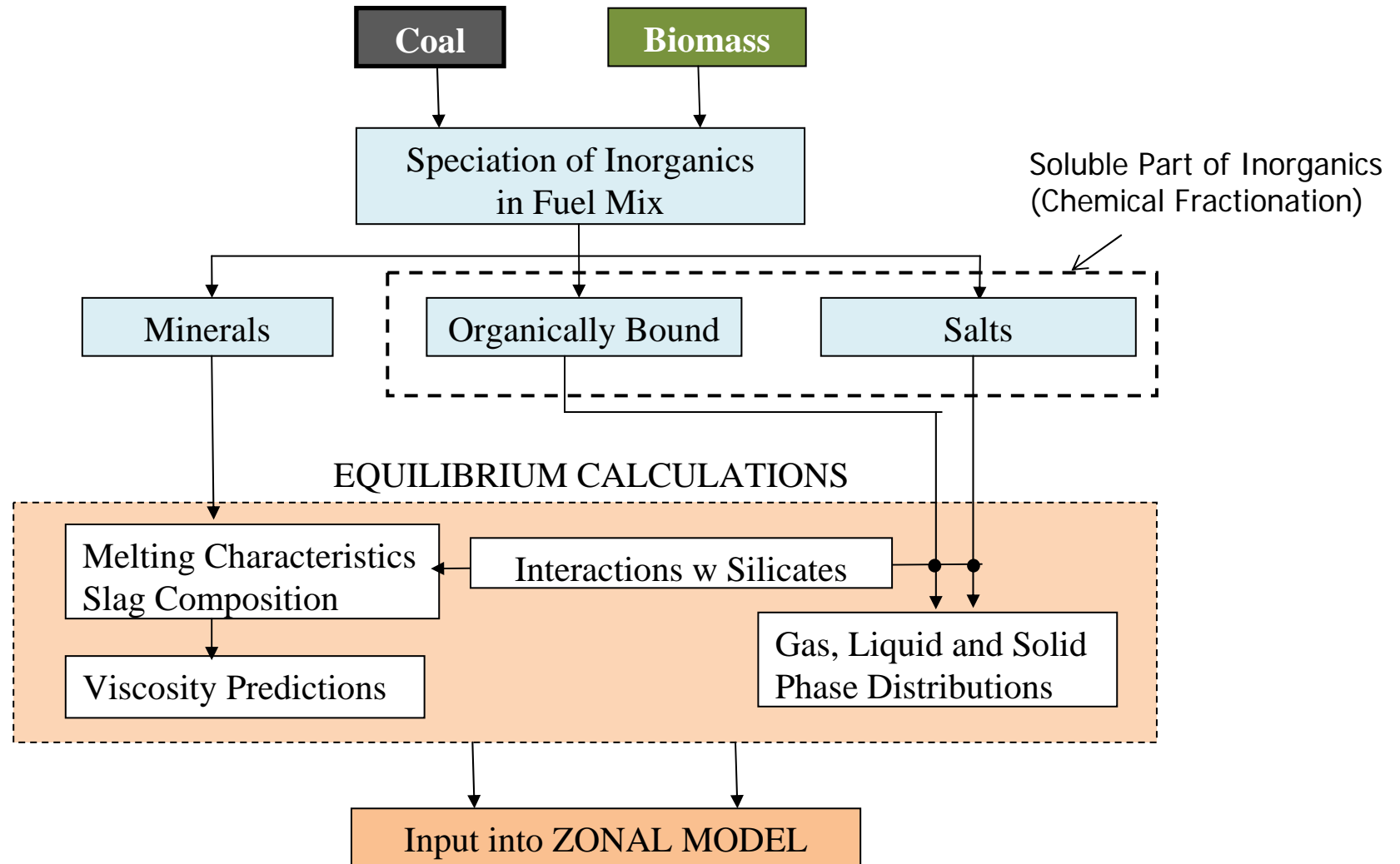
- Co-firing low percentages (up to 3<sup>th</sup>%) of high ash, dried sewage sludge may improve radiative heat transfer in the furnace, and thermal boiler performance! -> ash deposition?

NEXT -> ASH DEPOSITION CASES

## Steam parameters variations Sawdust Co-firing



# Ash Thermochemical Deposition Module



# Fuels Selection and Data Input Module

**SLAGGING PREDICTOR**

CARDIFF UNIVERSITY PRIFYSGOL CAERDYDD INSTITUTE OF ENERGY

BLEND CALCULATOR | BOILER | 1D TEMP PROFILE | SLAGGING/FOULING

Fuels | Ashes | Fuel Database | Deposit Database

Biomass

Fuels Selection: Danish Straw, T.

FuelName	MF	SF1	SF2
RS2	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>
SH1	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>
MG1	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>
WD1	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
MG1Wet	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
SD2wet	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
OR3	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
DS1	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
CS1	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
PC1	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
PK1	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
OR1	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
SD1	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>
SD2	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>
BC	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
OR4	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
SD3	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
DS2	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>

LHV: 14.67, Ash: 5.96

Primary Fuel, Sec Fuel 1, Sec Fuel 2, Sec Fuel 3, Sec Fuel 4

Proximate Analysis: Volatiles 68.49, Fixed C 13.15, Ash 5.96, Moisture 12.4, Total 0, L.H.V. MJ/kg 14.67

Ultimate Analysis: C 40.38, H 5.26, N 0.51, S 0.11, Cl 0.482

REA Phosphates Assessment: KH<sub>2</sub>PO<sub>4</sub>, % ash 4.34109, P<sub>2</sub>O<sub>3</sub> (FePO<sub>4</sub>) 0

Fuel Name: DS2

Ash Composition: SiO<sub>2</sub> 34, Al<sub>2</sub>O<sub>3</sub> 0.94, TiO<sub>2</sub> 0.06, Fe<sub>2</sub>O<sub>3</sub> 0.65, CaO 7.3, MgO 2, K<sub>2</sub>O 29.8, Na<sub>2</sub>O 0.85, SO<sub>3</sub> 4.74, P<sub>2</sub>O<sub>5</sub> 2.83, Mn<sub>3</sub>O<sub>4</sub> 0, Total 83.17

REA part: 0, 0, 0, 0, 90, 90, 95, 90, 0, 20, 0

PHOSP part: Ca\_phosphate 0, K\_phosphate 5

References: Danish Straw, T. Heinzel, Spilethoff, KRG Hein; Fuel Processing Technology 54 (1998) 109-125, H<sub>2</sub>O=8.04%

Memo2

Ash Fusion Temperatures: IT 0, ST 0, HT 0, FT 0

RadioGroup1:  Oxidized,  Red - oxy,  Reduced

Apply: OK, Normalise, Cancel, Save As

Fuel Type:  Coal,  Wood,  Agricultural Res.,  Sewage Sludge,  Meat Bone Meal

Calculate: Oxides, Elements, K Phosphate, Fe Phosphate

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\* Fe Phosphate only apply to Sewage SI  
\*\* K Phosphate not apply to SL, MBM

# Mechanistic Model

- Deposition of sticky ash particles  
-> inertial impaction

$$\dot{m}_d = u_f \cdot C_{ash,I} \cdot \frac{A_{tube}}{A_{total}} \cdot \theta \cdot p_{stick} \quad [kg / m^2 s]$$

$u_f$  – the bulk gas velocity

$C_{ash,I}$  – the mass concentration of ash particle

$p_{stick}$  – the sticking probability coefficient

$A_{total}$  – the total flow area

$A_{tube}$  – the cross-sectional area of the tubes perpendicular to the flow direction

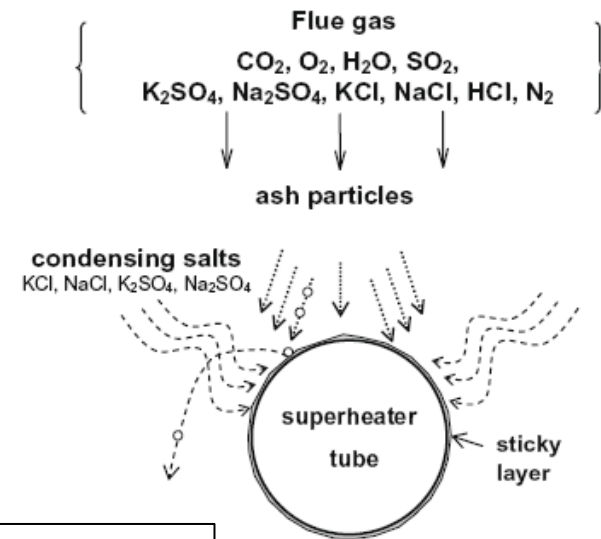


Fig. 2. Schematic presentation of ash particles deposition.

## Thermo-chemical Equilibrium Analysis

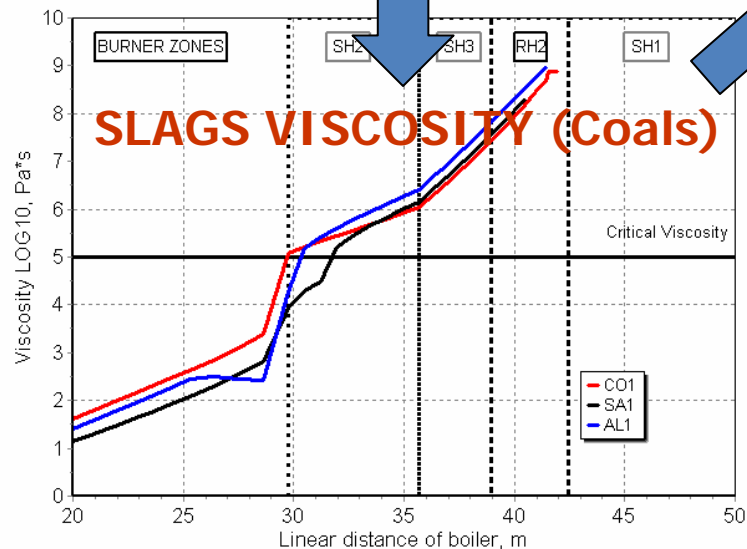
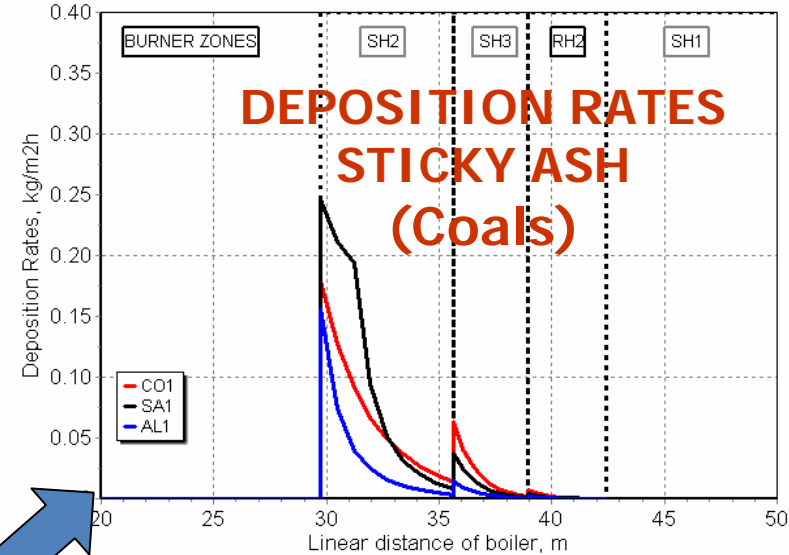
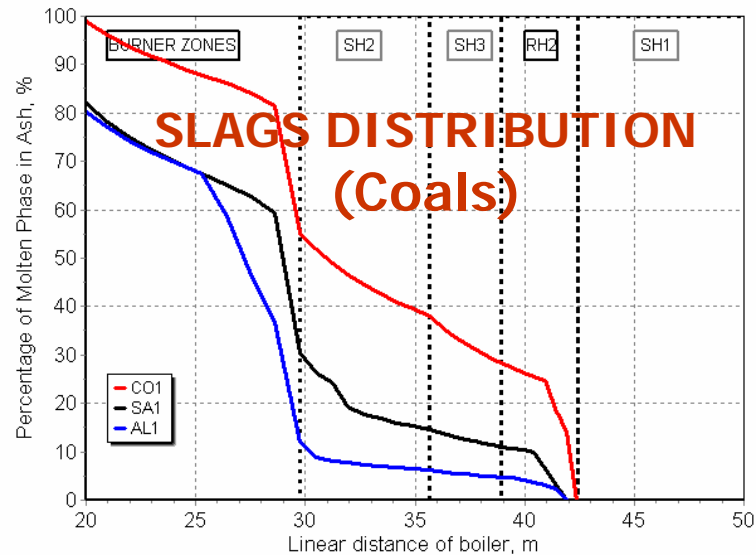
- Percentage of the molten phase in the approaching to the tube ash particles

$$\theta = \frac{m_{slag}}{m_{solid} + m_{slag}} \cdot 100 [\%]$$

- Sticking probability of the molten phase

$$p_{stick} = \begin{cases} \frac{\eta_{ref}}{\eta} & \eta > \eta_{ref} \\ 1 & \eta \leq \eta_{ref} \end{cases} \Rightarrow \eta_{ref} \approx 10^3 - 10^5 Pa \cdot s$$

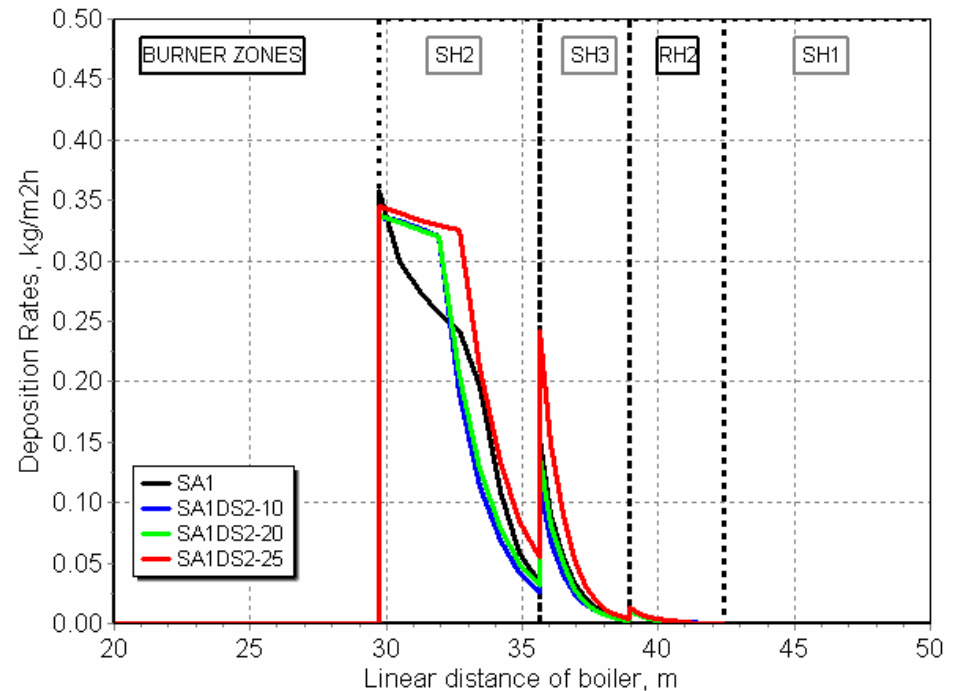
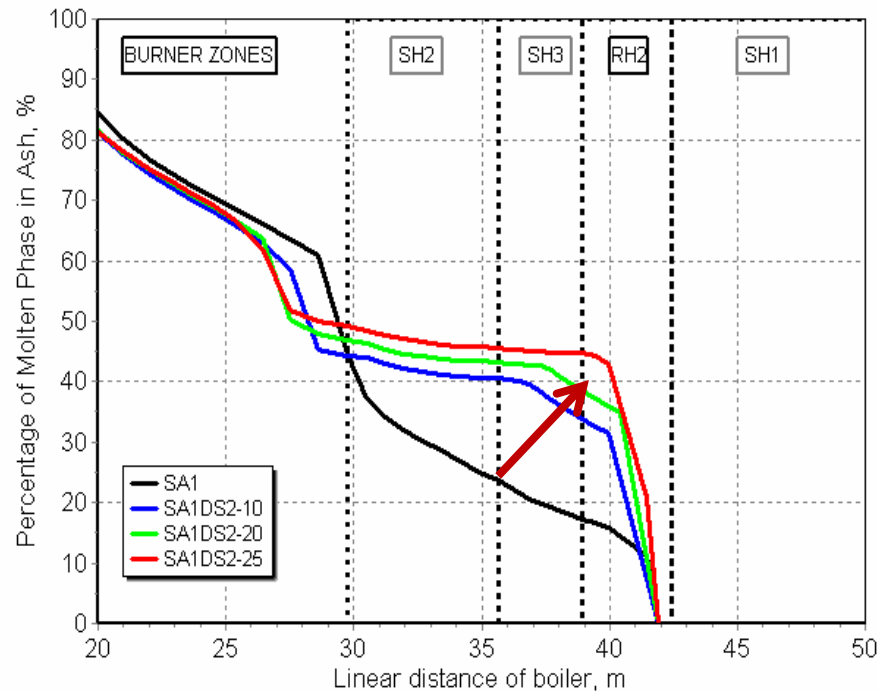
# Predicted Results for Pure Coals



- AL1 – best ash characteristics, but high ash content (erosion)
- CO1 – twice higher potassium content in silicates /clays, but overall low ash; slag distribution extended to the furnace outlet (resulting in increased ash deposition risk in the SH3 region)
- SA1 – intermediate ash content, and slag distribution



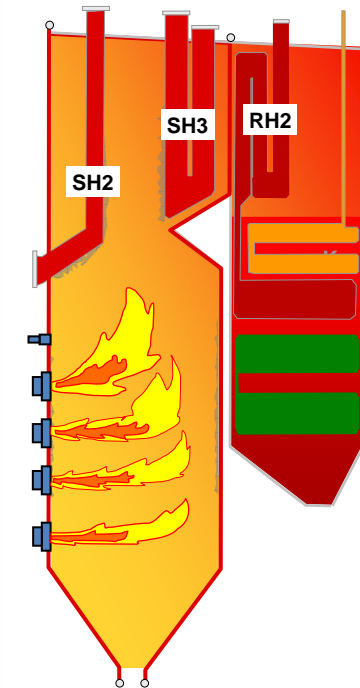
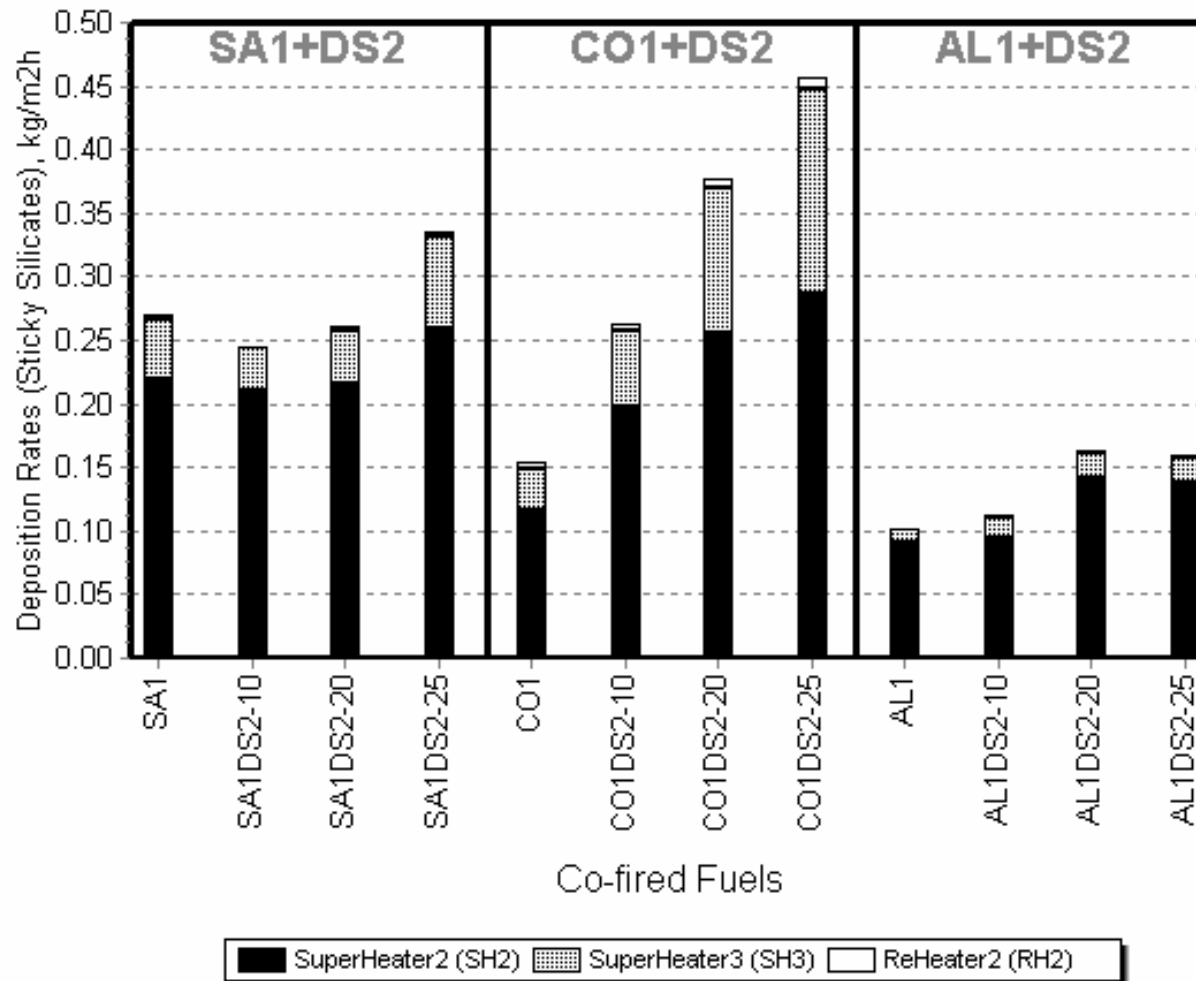
# Co-firing Straw with Coal



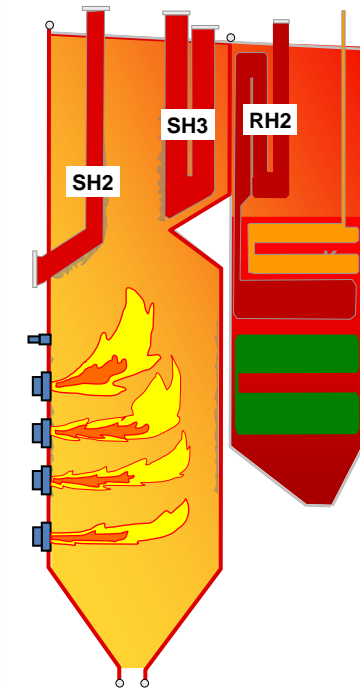
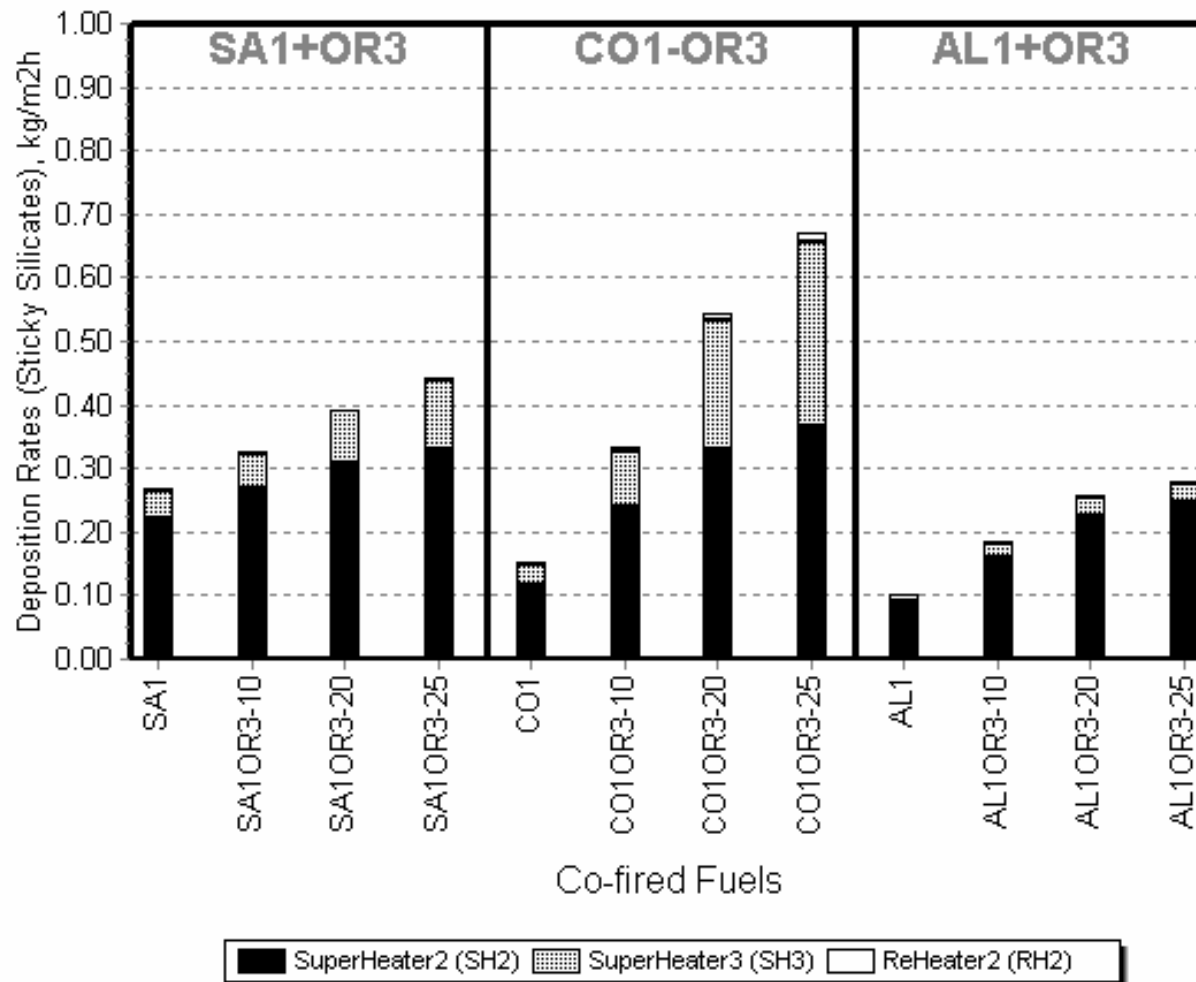
- Straw co-firing may change the melting characteristics of the viscous ash particles approaching the tube banks leading to the increase in ash deposition risk



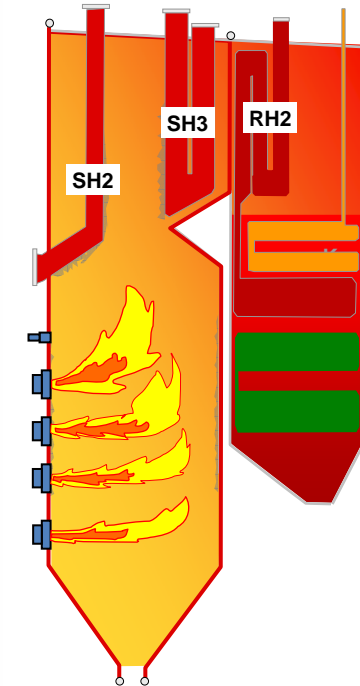
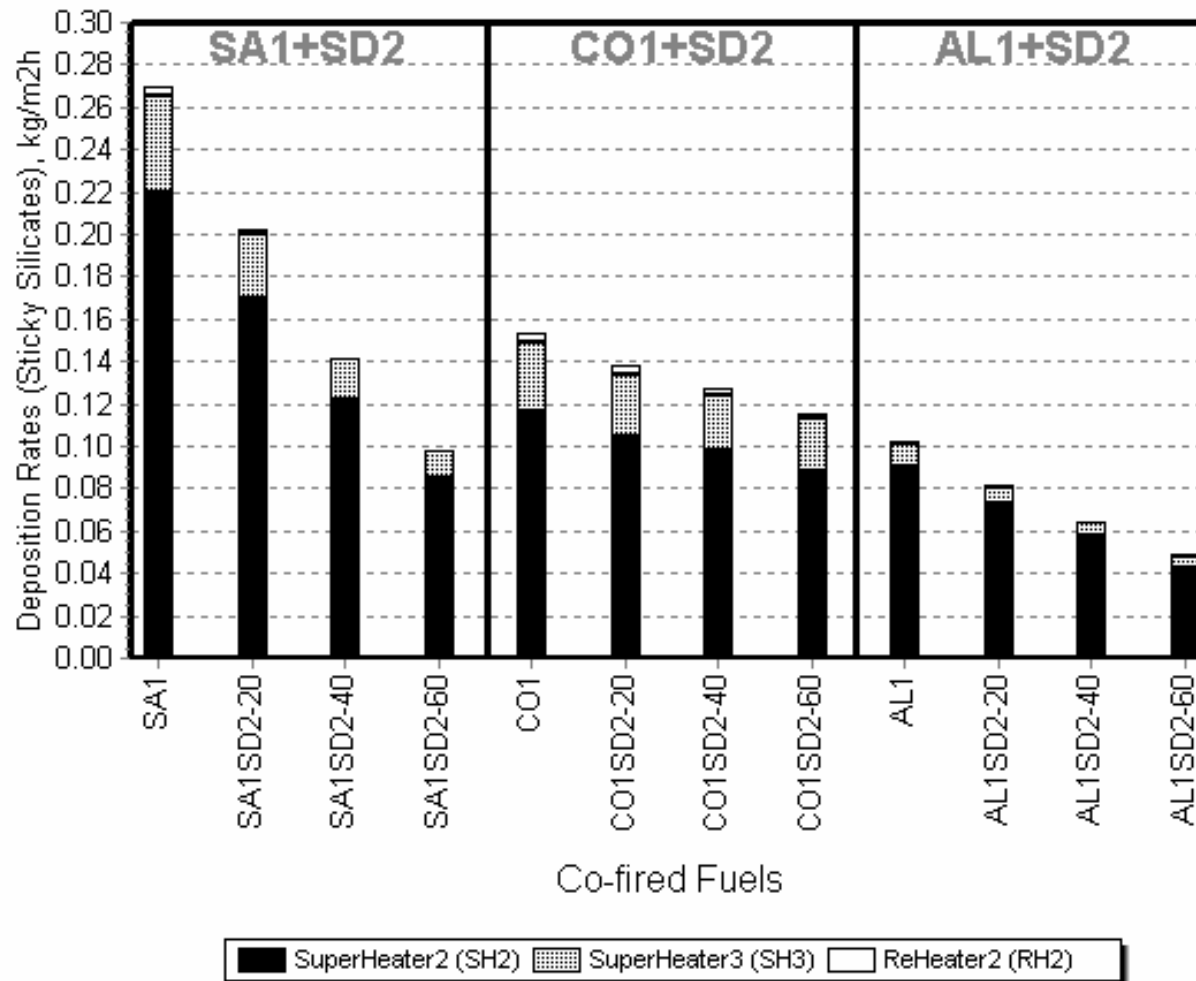
# Average Deposition Rates – Straw Co-firing



# Average Deposition Rates – Olive Residues



# Average Deposition Rates – Sawdust



# Mechanistic Model

- Salts Condensation / Deposition

An improved equilibrium model (based on FactSage data) was used to assess deposit formation risk originated from salts,

- Fate of Alkali Aerosols: Na, K (SO<sub>4</sub>/Cl)
- Formation of deposit binder - CaSO<sub>4</sub> (s),
- Assessment of the P<sub>2</sub>O<sub>5</sub>(g), Ca<sub>3</sub>(PO<sub>4</sub>)<sub>2</sub> (s) (phosphates)
- Risk of phosphoric acid H<sub>3</sub>PO<sub>4</sub>(liq) formation  
DeNO<sub>x</sub>- SCR poisoning
- HCl (g) concentration

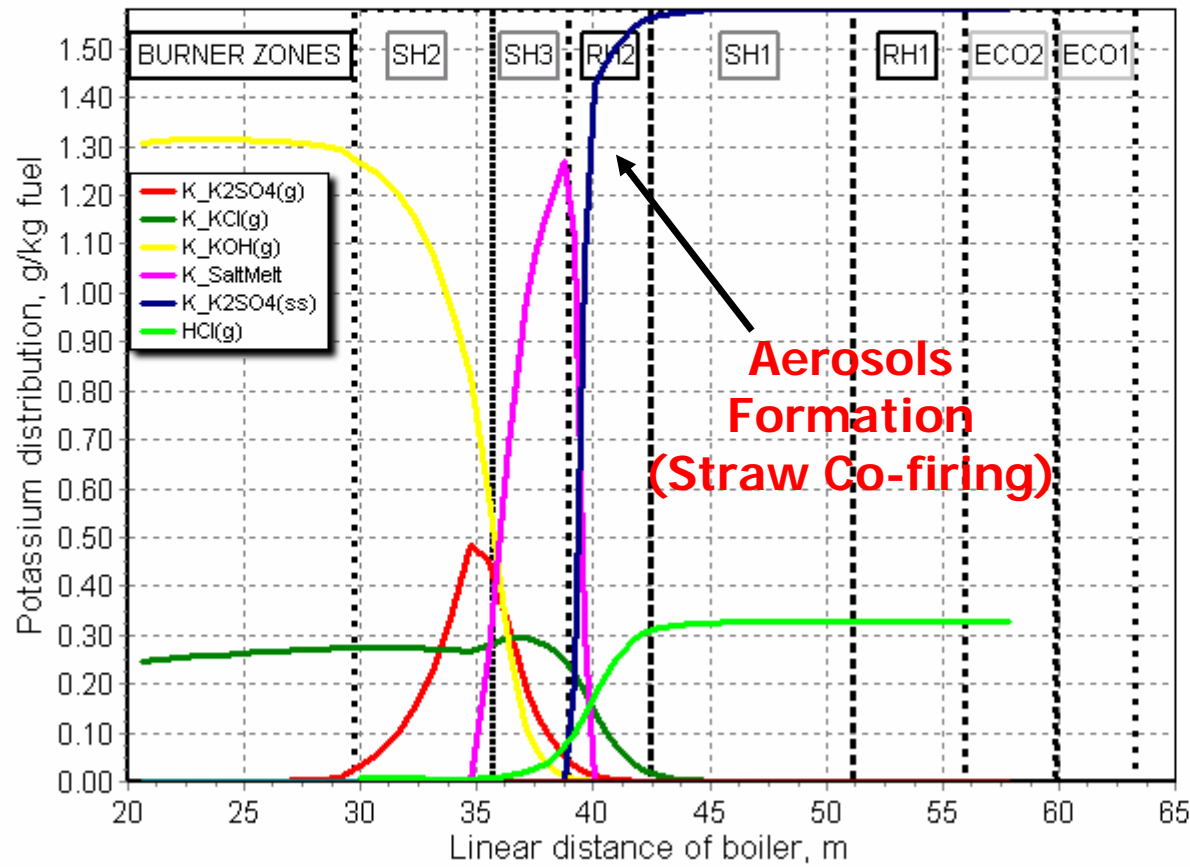


# SLAGGING PREDICTOR



BLEND CALCULATOR | BOILER | 1D TEMP PROFILE | SLAGGING/FOULING | SALTS DEPOSITION | HEAT TRANSFER | INDICATORS

Molten phase | **K distribution** | Na distribution | Sulphates/Phosphates



Co-firing Options

- Bi-Fuel
- Multifuel

Co-firing Rates, %

- Energy
- Mass

Parent Fuel

AL1

Substitute Fuel

WS1 10.0

Update

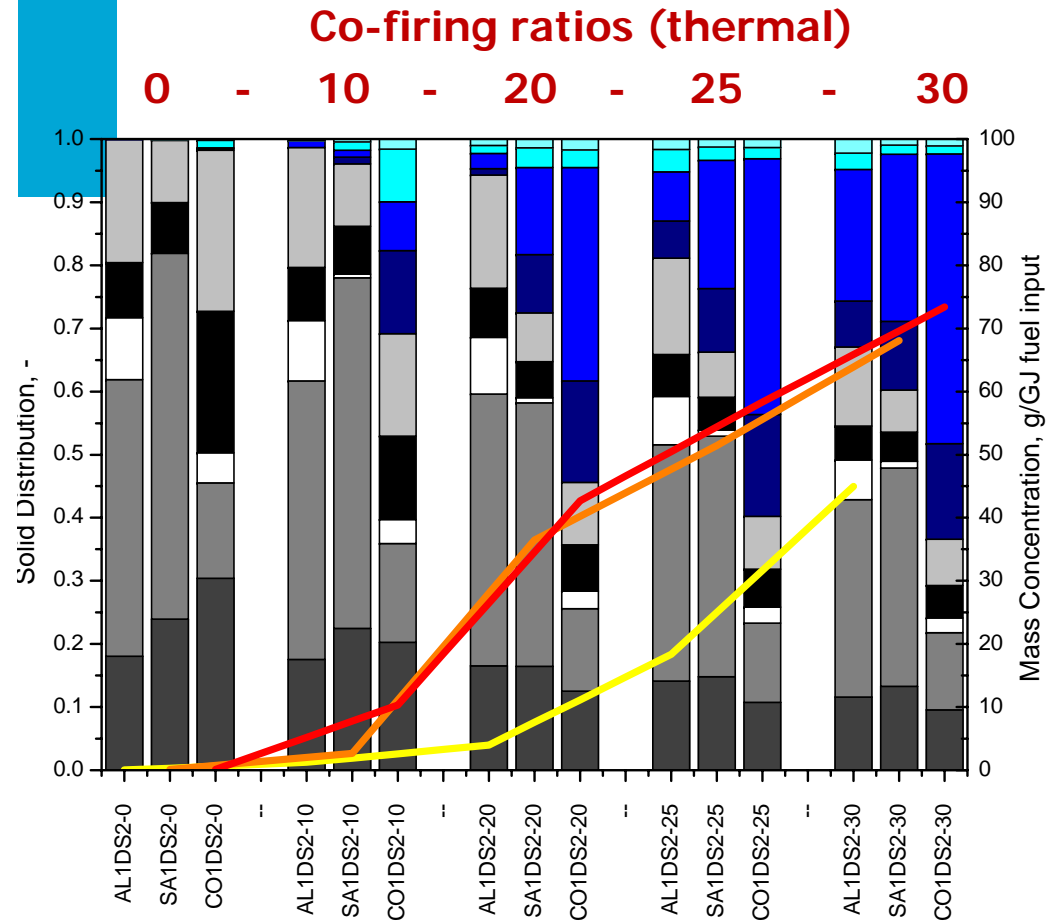
SLAGGING

**FOULING**

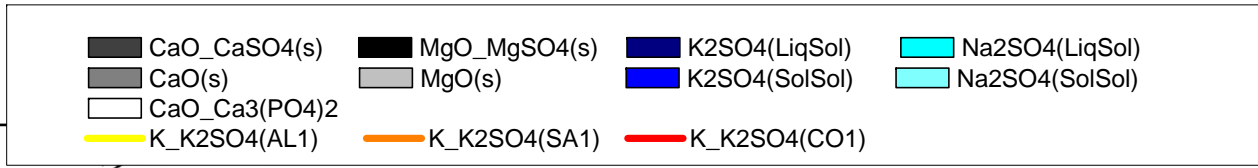
START

SETTINGS

# Salts Deposition Risk – Straw Co-firing



- Different coal ashes qualities studied (AL1, SA1, CO1)
  - High ash, low alkali content, AL1
  - Intermediate ash coal, SA1
  - Low ash, high alkali CO1
- Alkali metals interactions with Silicates/Clays considered
- **Buffering effect of AL1 Coal** – reduces alkali available for condensation -> captured by Si/Al ash particles
- Up to 30<sup>th</sup>% no chlorides in deposits



# Conclusions

- Co-firing with biomass may have a positive or negative impact on the ash deposition (non-additive behaviour).
- The quality of coal fired has a crucial role in reducing ash deposition when co-firing with high alkali salts biomass
- Interactions between biomass and coal inorganics may influence the viscosity of the silica-based ash particles leading to the increase in slagging risk
- The developed predictive tool is most useful for comparing the relative slagging/fouling performance of coals/biomass blends.
- Future work will focus on gathering deposition data to validate and improve simulations.

# Thank you for your Attention!

## Reference List:

- [1] Plaza P. et al., Use of a predictive model for the impact of co-firing coal/biomass blends on slagging and fouling propensity, *Energy & Fuels*, 23, 3437 – 3445, 2009
- [2] Plaza P. et. al., Zone modeling approach for the assessment of the effects of biomass co-firing on pf boiler performance, Paper to be presented and published on the 37<sup>th</sup> Clearwater Clean Coal Conference, 3-7June, Florida

## Contact:

**Piotr Plaza**, TU Delft / Faculty 3mE, Department of Process & Energy, Energy Technology Section, Leeghwaterstraat 44, NL-2628 CA Delft, The Netherlands  
Email: [P.P.Plaza@tudelft.nl](mailto:P.P.Plaza@tudelft.nl)  
Tel: +31 15 2782186